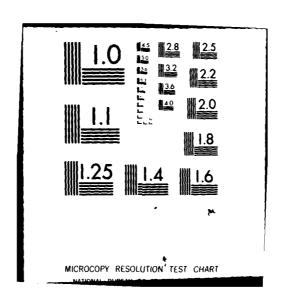
ARMY ELECTRONICS COMMAND FORT MONMOUTH N J AVIONICS LAB F/6 19/7 2.75 INCH ROCKET/AH-16 HELICOPTER MEAPONS SYSTEM BASELINE INSTR—ETC(U) APR 72 B ITRABASSI.E TOBONLA AD-A099 644 UNCLASSIFIED 1,2 ASSESSED TO



PHOTOGRAPH THIS SHEET AD A 0 99 644 DTIC ACCESSION NUMBER INVENTORY 2.75 INCH ROCKET/AH-1G HELICOPTER WEAPONS SYSTEM BASELINE INSTRUMENTATION TEST REPORT. VOLUME II. APRIL '72 DOCUMENT IDENTIFICATION DISTRIBUTION STATEMENT A Approved for public release! Distribution Unlimited DISTRIBUTION STATEMENT ACCESSION FOR NTIS GRALI DTIC TAB UNANNOUNCED **JUSTIFICATION** D DISTRIBUTION / **AVAILABILITY CODES** AVAIL AND/OR SPECIAL DIST DATE ACCESSIONED DISTRIBUTION STAMP 81 5 21 037 DATE RECEIVED IN DTIC PHOTOGRAPH THIS SHEET AND RETURN TO DTIC-DDA-2

DTIC FORM 70A

DOCUMENT PROCESSING SHEET

U. S. ARMY ELECTRONICS COMMAND

Fort Monmouth, New Jersey



2.75 INCH ROCKET/AH-1G HELICOPTER
WEAPONS SYSTEM
BASELINE INSTRUMENTATION TEST REPORT

VOLUME II

AIRCRAFT INSTALLATION and TEST TECHNICAL AREA
AVIONICS LABORATORY

By Benjamin Tirabassi and Edmund Tognola

April 1972

DISTRIBUTION STATEMENT A

Approved for public release; Distribution Unlimited

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FIG.	11	Pitch Angle of Attack Data	.75
FIG.	12	Yaw Angle of Attack Data	
FIG.	13	Yaw Angle of Attack and Gyro Yaw	
FIG.		Horizontal LVDT Analysis	
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FIG.	_ `.	LVDT (LHF)	
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والأحالي بمقامعه ومعاملا معاورة والمارين فأراها

1.0 Data Format

The output data from the Data Acquisition Unit was recorded on a Leach Model 3200 digital magnetic tape recorder in a bit parallel pulse code modulated (PCM) format as shown in Figure 1.

Recorder Tape Track	Function
1 2 3 4 5 6 7 8 9 10 11 12 13 14	Not Used Parity Sign Bit 10 (MSP) Eit 9 Bit 8 Bit 7 Word Mark Bit 5 Bit 4 Bit 3 Bit 2 Bit 1 (LSE) Bit 6 Not Used Range Time (Pulse /mplitude Fieddulated)

FIG. 1

For ease of presentation, the reproduced data is usually printed in a block format consisting of 120 words as shown in Figure 2. The words are written on the tape in a sequence that occurs by reading the data frame left to right, row by row. The data frame represents one complete sampling cycle by the Data Acquisition Unit (DAU). The DAU transmits the equivalent of 100 data frames per second to the recorder. Words S1 and S2, the synchronization words, are used to determine the frame structure. During the decommutation and formatting process, the computer searches the continuous data stream until the synchronization words are located. The computer then starts with the next data word and blocks the data into the desired 120 word format.

The Phase A and Phase B instrument configurations for the data presented in this volume are indicated in Figure 3 and Figure 4 respectively. The configuration charts list the assigned data words and engineering unit dimensions for each monitored parameter. The required measurements, necessary for performing the data analysis, are shown in Figure 5.

2.0 Recorded Data Conversion

2.1 Sample Octal Printout

A typical octal data listing is shown on pages 6 through 15. The computer printout represents the data recorded as Run #138 on 24 August 1971. The recorded Phase B data extends for a period of 0.52 seconds immediately following the occurrence of avent marker #1 which signals the aircraft approach to the rocket release point.

AI	A 2	A3	44	A 5	46	A7	BI	CA	CD	Bii	01
AI	A 2	A3	A 4	A5	A 6	A7	B2	CA	CO	B12	02
Ał	A2	A3	A4	A 5	A 6	A7	83	CA	CD	813	D3
Al	12	A 3	44	A 5	A 6	47	84	CA	CD	814	D4
Al	AZ	A 3	A4	A 5	A 6	A7	B5	CA	CD.	B 15	05
Al	A 2	A 3	A 4	A 5	A 6	A7	86	CA	CD	816	CI
AI	A 2	À 3	A4	A5	A 6	A7	87	CA	CO	817	C2
AI	A 2	A 3	A4	A5	A 6	A7	88	CA	CD	818	CAL
AI	A2	A 3	A4	A5	A 6	A,7	89	CA	CO	ETI	ET2
ΑI	42	A3	A 4	A 5	46	A7	B10	CA	CD	\$1	\$2

DATA	INPUT CHANNELS	. DAU GENE	ERATED INFORMATION
WORD	INPUT	WORD	FUNCTION
A1 - A7	HIGH RATE ANALOG	ETI - ET 2	ELAPSED TIME CODE
8! - 83	SYNCHRO	CAL	CALIBRATION WORD
84 - BI8	LOW RATE ANALOG	S1 - S2	SYNCHRONIZATION WORD
DI	FLIGHT TEST RUN CODE		
D 4	EVENT MARKERS		

NOTE ALL OTHER WORDS ARE UNUSED.

FIG. 2 DAU DATA FRAME

PHASE A CONFIGURATION

SENSOR	WORD	DIMENSION
IR Detector (Left)	Al	volts
Lateral Accelerometer	A2	ft/sec ²
Vertical Accelerometer	٧3	ft/sec ²
Fore/Aft Accelerometer	Λ4	ft/sec ²
IR Detector (Right)	A5	volts
Roll Rate	A6	dearees/second
Yaw Rate	A7	degrees/second
Aircraft Pitch	ВТ	degrees
Aircraft Roll	B2	degrees
Aircraft Yaw	В3	degrees
Pitch Rate	B4	degrees/second
Angle of Attack* (#2LY)	B5	degrees
Angle of Attack (#2LP)	B6	dearces
Angle of Attack (#4RY)	E7	degrees
Angle of Attack (#4RP)	88	degrees
Angle of Attack (#3NY)	B13	denrees
Angle of Attack (#3NP)	B14	degrees
Angle of Attack (#1LY)	B15	degrees
Angle of Attack (#1LP)	B16	degrees
Angle of Attack (#5RY)	817	degrees
Angle of Attack (#5RP)	B18	degrees

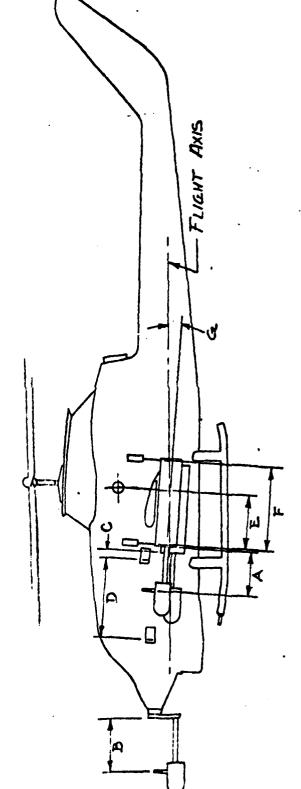
^{*}Key for Angle of Attack Transmitter Position

L - Left	#1 Outboard
R - Right	#2 Inboard
!! - Nose	#3 Nose
Y - Yaw	#4 Inboard
P - Pitch	#5 Queboard

PHASE B CONFIGURATION

SENSOR	WORD	DIMENSION
IN Detector (Left)	AT	volts
Lateral Accelerometer	.12	ft/sec ²
Vertical Accelerometer	V3	ft/sec ²
Fore/Aft Accelerometer	A4	ft/sec ²
IR Detector (Right)	A5	volts
Roll Rate	A6	degrees/second
Yaw Rate	A7	degrees/second
Aircraft Pitch	B1	degrees
Aircraft Roll	B2	degrees
Aircraft Yaw	B3	degrees
Pitch Rate	B4	degrees/second
LVDT* (LHF)	B5	inches
LVDT (LVF)	B6	inches
LVUT (LHA)	57	inches
LVUT (LVA)	В3	inches
LVOT (RRF)	89	inches
LVUT (RVF)	013	inches
LVUT (REA)	611	inches
LVDT (RVA)	B12	inches
Angle of Attack (Hose-Yaw)	B13	degrees
Angle of Attack (Nose-Pitch)	B14	degrees
Angle of Attack (Left-Pitch)	B15	dearees
Angle of Attack (Left-Yaw	816	degrees
Angle of Attack (Right-Pitch)	B17	denrees
Angle of Attack (Right-Yaw)	B18	derrees

^{*}Key for Linear Variable Differential Transforms L-Left, N-Horizontal, F-Forward, R-Right, V-Vertical, A-Aft



DIMENSION	DISTANCE
K & O C	9 3/4 Inches 25 Inches 4 3/4 Inches
E*('leasured from Rotor Shaft)	28 Inches 59 Inches
G Mose AAT to Outboard AAT	80 Mils 159 Inches
Nose AAT to Inboard AAT Launcher Length	156 Inches 60 5/8 Inches

*Varies slightly between LVDTs

FIG. 5 SENSOR LOCATION MEASUREMENTS

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2.2 Octal to Binary Data Conversion

The computer converts the 12 bit binary words, as recorded on the magnetic tape, into an octal representation during the decommutation and formatting process. It is often necessary to be able to reconstruct the binary word from the octal printout or to determine the octal data word from binary representation indicated on the data acquisition testset. The binary data word is represented by a parity bit, sign bit and ten data bits as indicated below:

In order to convert the binary data to an octal form, the bits are divided into groups of three.

The right most bit of each group is given a weight of 1. The center bit is given a weight of 2 and the left most bit of the group is given a weight of 4. The weights within each group are then added to give the octal representation. As an example the binary data word snown below will be converted into an equivalent octal word:

Binary Data Word: 111011100100

The reverse process is used to convert the data from octal to binary. An example is shown below:

The weights of the bits are shown below the lines.

The resulting data bits are shown below.

$$(\underline{1} \ \underline{0} \ \underline{0}) \qquad (\underline{0} \ \underline{0} \ \underline{1}) \qquad (\underline{0} \ \underline{0} \ \underline{0}) \qquad (\underline{1} \ \underline{1} \ \underline{1})$$

and the binary word is 100001000111.

2.3 Binary to Analog Data Conversion

A binary data word is shown below:

Parity, Sign, Bit 10, Bit 9, Bit 8, ... Bit 1.

The data acquisition system converts the analog input into a digital representation with each bit representing 2^{k-1} counts with H being equal to the bit number. System sensitivity is set at 5 volts = 1000 counts. A one (1) in the sign bit position represents a negative analog sense. The following binary data word is reconverted back to the original input voltage as an example:

Data Word 0 0 1 0 0 0 1 0 1 1 1 0 Bit Position P S 10 9 8 7 6 5 4 3 2 1

The total number of counts becomes $(0 \times 2^0) + (1 \times 2^1) + (1 \times 2^2) + (1 \times 2^3) + (0 \times 2^4) + (1 \times 2^5) + (0 \times 2^6) + (0 \times 2^7) + (0 \times 2^8) + (1 \times 2^9) = 558 \text{ counts}$

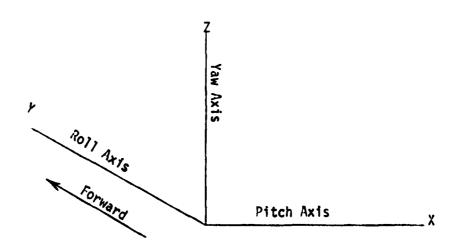
The analog voltage represented by the binary word is equal to: 558 counts X 5 mv = +2.790v count

The data acquisition system uses an odd parity format. The parity bit becomes a 1 in order to make the number of bits in the word equal to an odd number. The parity bit therefore becomes a bit check on the data word. If the data word has no parity, yet has an even number of bits in the word then the word is in error and should be disregarded.

The sign bit represents the sign of the analog input to the data acquisition unit and may not be consistant with the desired coordinate system. Therefore, the sense of each transducer must be checked and sign conversion performed by the computer, if the sense is not proper.

2.4 Coordinate Determination

The coordinate system used in the analysis of the flight data is shown below.



The sense of the transducer output voltage is shown below in Figure 6.

Sensor	Sense	Direction
Yaw Gyro	+	CW (Negative Z Axis)
Pitch Gyro	+	Up (Positive X Axis)
Ro11	+	CCW (Negative Y Axis)
Yaw Rate Gyro	+	CW (Negative Z Axis)
Pitch Rate Gyro	+	Down (Megative X Axis)
Roll Rate Gyro	+	CCW (Negative Y Axis)
Fore/Aft Accelerometer	+	Fore (Positive Y Axis)
Vertical Accelerometer	+	Down (Negative Z Axis)
Lateral Accelerometer	+	Left (Negative X Axis)
Angle of Attack Transmitters	Maximum	CCW (*)
Linear Variable Differential Transformers (AC #67-15691)		
Left-Vertical-Forward	+	Up (Positive Z Axis)
Left-Vertical-Aft	+	Up (Positive Z Axis)
Right-Vertical-Forward	+	Down (Hegative Z Axis)
Right-Vertical-Aft	+	Down (Negative Z Axis)
Right-Horizontal-Aft	+	Right (Positive X Axis)
Right-Horizontal-Forward	+	Right (Positive X Axis)
Left- Horizontal-Forward	+	Left (Negative X Axis)
Left- Horizontal-A£t	+	Left (Negative X Axis)

^{*}Axis alignment varies with configuration Note: Sense Readings taken at DAU Control Unit.

FIG. 6 SENSOR DATA SENSE

2.5 Transducer Scale Factors

The analog transducer scale factors are shown in Figure 7.

The scale factors are used to determine the response of the sensor knowing the analog output.

Sensor Type	Scale Factor
Angle of Attack Transmitters	12.5 degrees/volts*
Linear Variable Differential Transformers	0.32 inch/volt
Accelerometer	1.25 G/volt
Rate Gyros	10 degrees/second/volt
Position Gyros	18 degrees/volt

^{*}Average value for all transducers

FIG. 7 Transducer Scale Factors

2.6 Engineering Units Determination

A representative number of octal data words are converted into engineering units in Figure 8. The word number position can be seen in Figure 2 and the assigned parameter sensor can be determined from Figure 4.

The sample data frame being converted immediately follows the range time printout 236 0732 02.823 on the octal listing. The conversion of the octal word to a binary representation was performed as discussed in paragraph 2.2. The digital counts and analog outputs were determined using the technique discussed in paragraph 2.3. The scale factor for each of the applicable transducers was indicated in Figure 7. The resulting engineering units are shown in Figure 8 and compare with the data frame printout on page 49.

3.0 Engineering Units Printout

3.1 Phase A Data

The data presented on pages 22 through 47 is a segment of the data recorded for a Phase A flight test. The data, from Run #35 (recorded as octal 43), represents the data accumulated for a period of one second during the "straight and level" segment of the flight.

		ista Hord	Digital	Output 65my/count		Engineer	
Mord	Octal	Binary	Counts	(volts)	Scale Factor	ing Units	Remarks
િલ (સ	4036	011 110 000 011	30	.150	:lone	4036	Noise Level, No Trigger or IR Pulse Present
A2	2014	010 000 011 100	12	090*-	32.2ft/sec ² /volt -2.4l ft/sec ²	-2.41 ft/sec ²	Sign Change Re- quired for Proper Coordinates Chan- nel Calibration .8 volt/q
A3	4314	100 011 001 100	204	1.020	32.2ft/sec ² /volt 41.01 ft/sec ²	41.01 ft/sec ²	Sign Change Required for Proper Coordinates Channel Calibration 8 volt/g
A4	4074	100 000 111 100	09	008°.	32.2ft/sec ² /volt 12.06 ft/sec ²	12.06 ft/sec ²	Channel Calibra- tion .8 volt/g
75	0010	000 000 000 000	8	.040	None	0100	Noise Level, No Trigger or IR Present
йб	4072	010 111 000 001	28	.290	10°/sec/volt	2.9 deg/sec	Sign Change Re- quired for Proper Coordinates
ii.7	4030	100 000 011 000	24	.120	10°/sec/volt	1.2 deq/sec	Sign Change Re- quired for Proper Coordinates
181	1909	110 000 110 001	65	245	18°/volt	-4.41 deg	
B2	0005	010 000 000 000	2	.010	l3°/volt	+.180 deg	Sign Change Re- quired for Proper Coordinates

FIG. 8 OCTAL TO ENTINEERING UNITS CONVERSION

	Remarks	Sign Change Re- quired for Proper Coordinates	Sign Change Re- quired for Proper Coordinates	Sign Change Re- quired for Proper Coordinates	2 volts & 0°	2 volts % 0°	Run #138			Sign Change Re- quired for Proper Coordinates
Fnaineer	ing Units	+.180 deg	+4.00 deg	075 in	4.60 deg	-9.4 deg	138	017	.01	.038
	Scale Factor	18°/volt	10 deq/sec/volt	.32 in/volt	12.5°/volt	12.5°/volt		.32 in/volt	.32 in/volt	.32 in/volt
Output @5mv/count	(volts)	.010	.400	235	1.805	1.510		055	+.035	+.120
Digital	Counts	2	80	47	198	302	138	11	7	24
Data Word	Binary	010 000 000 000	100 001 010 000	110 000 101	100 001 101 000	000 100 011 110	010 000 010 000	110 000 000 011	111 000 000 000	100 000 011 000
	Octal	£000	4120	6057	0551	0436	0212	6013	2000	4030
	hord	63	54	53	ยา3	814	63	5.6	69	B1 0

FIG. 8 OCTAL TO ENGINEERING UNITS CONVERSION (CON'T)

EMPREERING CHITS CRIMINAL (PRISE A)

. •	1 1 1			4166	· · · · · · · · · · · · · · · · · · ·			# (a) (b) (b) (c) (c) (c) (d) (c) (d) (d) (c)	1 4 4 10 6 10 4	000 000 000 11	# 0 C 1 4	
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			() ()	(*) (*) (*)	7,4577	6 4	7 . C . W. I	1665	4034	-4.743	6763	
15	C(• • • • • • • • • • • • • • • • • • • •	n € 6	277	0 7 0 0 0 1	-0.720	4534	5605	4006	+633	4030	
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4936	3.960	-25	-1.280	7055	-0.830	-0.720	-0.322	2605	9004	-0-194	000+	
000		- 20	-1.600	+322	-0-760	-0.580	-5.C9C	2505	4086	9-182	4030	
0004	-0.490	1	600 0	220-	10.543	069-0-	-2-328	2605	4306	-1.988	4000	
7 6	062*1-	1 (0.150	275	024.0	0.580	-6.638	2605	9004	-9-678	2000	
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20.3643			•									
6333	(44.1-	•	4.6.3	+022	-3.353	0.963	-3.150	2605	4004	-0-190	*	
153	C7++-	7.	5.550	+925	0-0-0-	-0.646	-0.1.0	2605	4536	-0.276	40.00	
£00 4 - ₹	-04167		6.27D	4922	-0.043	-0.580	-0.276	2605	4004	0.453	\$000	
	3.320		0.E.	4022	0.0	0.690	095	2665	4004	-7.836		
9	1044		11 250	4022	0.01	02/-0-	-0.322	CB97	900	-0.259	000	
4370	1.760	3.056	10,550	4022	-6.123	-3.763	-0-328	26.35	900	-1-888	9004	
4 233	1.760		11.593	4022	-0-160	-0-160	-6.C38	2605	4004	-9.743	4524	
0.03 0.03	1-120	Ä	12.220	4322	-0.250	071.0-	4005	2605	900	4003	4900	
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											-	
6,474,5												
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-	-2-090	- 2	7.550	4 322	-0.360	-0.580	061.0-	2605	\$00 3	-0.270	0007	
- 1	-4.320	-26	2.110	+622	-0-390	-0.63¢	-0-210	2005	9004	0.453	0007	
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464	-1.18	-27.	1.120	4055	0.0	-0.520	•	2605	4004) 	

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-5-5-5- -0-328 -0-428 -0-428
0.320
0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -
#
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- 36-17-0 - 26-17-0 - 26-95-0 - 27-95-0 - 27-95-0
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The analysis presented in paragraph 4.1 was performed on the data shown in the engineering units printout plus the data recorded in the succeeding two second period.

The data from the entire run is available on IBM compatible 9 track tape. Small representative samples were printed in engineering units in order to verify that the data was recorded, decommutated, converted and formatted properly.

3.2 Phase D Data

The engineering units printout shown on pages 49 through 62 is from a Phase B test flight flown on 24 August 1971. The sample of data shown represents the data collected for a period of approximately 1/2 second.

The fourth engineering units data frame on page 49 is the sample data frame converted from the octal data as described in paragraph 2.6.

The data used for the analysis, performed in paragraph 4.2 and 4.3, on the LVDTs and accelerometers was part of a "straight and level" flight from Run 138.

4.0 Subsystem Validation

The following paragraphs present an analysis of retrieved data samples employing various statistical techniques for the purpose of verifying the performance of the airborne instrumentation.

Statistical operations were performed to obtain the data averages, RMS values, frequency spectrum profiles (Fourier analysis) and correlation between sensor data for the angle of attack transmitters, linear variable differential transformers and the inertial reference system accelerometers. The relative tracking of the above mentioned sensors is illustrated in X-Y plots of the retrieved data.

Analysis was performed on the trigger and IR detector data to determine the firing delay characteristics of the rocket system and the average velocity of the 2.75" Rockets.

All statistical calculations were performed on an IBM 360 computer.

4.1 Angle of Attack Transmitter Analysis

A sample of the data used for the analysis of the angle of attack transmitters (AAT) for Run 35 is shown on pages 22 through 47. The data upon which the analysis was performed was recorded during a Phase A Configuration 2 flight on June 23, 1971. The sample was retrieved during a one second period. The analysis was performed upon this data and the data in the succeeding two second interval.

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404	-8.24	C4.1.4-	15.88	4011	-2.450	0.800	-7.050	5412		0	4000
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13.75   14.27   401   -1.400   -0.007   5412   15 5.21   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.25   15.		~		-1.150	-1.000	-0.035	5412	<del>-1</del>	-2.54	4000	
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The angle of attack data was corrected prior to the analysis for the mounting alignment of the AAT pods. The engineering units listing is in an uncorrected form.

### 4.1.1 Data Statistics

Results of the angle of attack statistical analyses are shown in Figures 9 and 10.

Due to the physical mounting of the angle of attack transmitters, correction factors have been applied to the data in order to compensate for the mounting offsets. The nose pod was pitched upward by 8 mils and was angled to the right by 7.5 mils. These offsets were converted to correction factors of 0.450 degrees for the nose pitch and 0.421 degrees for the nose yaw. The correction factor for the nose pitch was subtracted from the data and the correction factor for the nose yaw sensor was added to the sensor data prior to the analysis. The four launcher pods were all pitched upward by 80 mils. This offset, equivalent to 4.499 degrees, was subtracted from the pitch angle of attack readings.

The mean values for each of the pitch angle of attack transmitters and the pitch gyro are shown in Figure 9. These values indicate the average reading for the sensors over the period of the sample.

The root-mean-square (RMS) values for each of the parameters were calculated to indicate the degree of excursion of the data. The RMS values for the sensors fell in a range within 0.1 of the absolute value of the mean values. This indicates that most of the data samples fell within a very narrow range of mean value.

The standard deviation was calculated in order to provide a measure of the data dispersion. For a normal distribution, the standard deviation or  $\pm \sigma$  indicates the range in which 68.2% of the samples were located about the mean. For the angle of attack sensor in the Pitch #1 position, 68.2% of the samples were within  $\pm$ .9150° of the mean value (-5.7427°).

A two sigma value (2 $\sigma$ ), or twice the value of the standard deviation, indicates the data band in which 95.5% of the samples fell. A 3 $\sigma$  value indicates the data band in which 99.7% of the values were located. For the above example, this would indicate that 95.5% of the value are within  $\pm 1.830^{\circ}$  of the mean and 99.7% are within  $\pm 2.745^{\circ}$  of the mean. It will be shown later in the Fourier Analysis Section that the predominant portion of the data excursion is cyclic and in fact these deviation measurements are accurate vibratory motion induced sensor readings.

The variance, which is equal to the square of the standard deviation, is a measure of the range of the data and presented in Figure 9.

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CYRD WITCH -0.	0.3477	-6.3950	-0.5556	-0.3853	4264.0-	1.0000	

FIG. 3

ANGLE OF ATTACK SENSORS

				:			
GYRE YAN	156.2-	1.122	0.632	0.399	:	1.0000	
YAN S	19.5897	9.6057	0.5244	0.2750		1.0000	
7 64 4	-0-3629	0.4839	0.3202	0.1025		1.0000	!
VAN 3	1-1962	1.4740	9.8750	0.7656		1.0000 0.9256 0.9274	1
YAM 2	-0.5372	0.6456	0.3958	6.1598	:	1.0000 0.7870 0.8070 0.95 %	
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F16. 10

Similar data analysis is presented for the yaw angle of attack transmitters and the yaw gyro which is shown in Figure 10.

## 4.1.2 Data Correlation

A computer program was written to assess the degree of correlation between data signals and calculate correlation coefficients to measure data confidence level. The results of the analysis are shown in Figures 9 and 10 for the pitch and yaw sensors, respectively. The correlation between the pitch angle of attacks was very good with a .8631 coefficient between Pitch #1 and Pitch #3 being the lowest. Pitch #3 was located on the nose of the aircraft and sensed the airflow approximately 0.12 seconds earlier then the launcher sensors. This would be a contributing factor to the lower correlation factor.

The lowest correlation factor between the pitch sensors #1, 2, 4, 5 was 0.9415 and the highest factor was 0.9864. The high correlation between these sensors indicates that the angle of attack transmitters were responding to the airflow and the relative tracking movements of the individual sensors were in near perfect agreement.

The correlation between the gyro pitch and the angle of attacks was very poor. This indicates that the helicopter flight profile was not effected by the cyclic change in airflow pattern. Reviewing the engineering units printout shows that the pilot was able to maintain his pitch attitude even though abrupt changes in the airflow occurred.

Identical information is available for the yaw angle of attack in Figure 10. From the mean values it can be seen that the airflow around the aircraft was almost symmetrical and indicates a streamlining effect with relative wind flowing down and outboard of the fuselage.

# 4.1.3 Frequency Spectrum Determination

A standard computer subroutine was used to analyze the frequency content of the various recordings. This operation calculates the Fourier coefficients over one cycle. Based on previous observations, the fundamental frequency of these signals is 11 Hertz (period equals .09 seconds) and corresponds to the natural helicopter rotor frequency. Since the data acquisition system records at a rate of 100 samples per second, then 9 data points are necessary for a calculation. For each parameter, separate calculations were made for consecutive blocks of nine data points. The results of these calculations are shown on pages 67 through 74.

The accuracy of each DC component can be verified by checking the 9 appropriate data points. Since the AC variations of these signals are quite low, then the Fourier coefficients are correspondingly low. It can be noticed in the pitch calculations for data points 181 to 189, there was a significant increase in the magnitude of the coefficients. Referring to the plot of the pitch signals in Figure 11, it is seen

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0-040	0.0326	0.0716	0.0412	0.0401	0.0209	-0.0026	-0.0000	-0.0348	-0.0140	-0.0945	0.0067	-0.0201	-0.0173	-0.6729	-0.0982	0.0215	-0.0698	-0.0300	-0.0000
0.0688	0.0000	0.2596	0.0898	-0.0268	0.0453	01,000	0000	-0.0542	1600.0-	-0.3263	0.0360	0.0392	0.0173	-0.1011	-0.1598	-0.0172	-0.0579	0.0108	0.0000
0.0206	0.0153	0.0659	0.0492	0.0223	0.0038	0.0072	000000	-0.0224	-0,0312	-0.0879	0.0369	-0.0111	0.0100	-0.0611	-0.1378	-0-0064	-0.0334	-0-0018	0.0000
-0.0072	0.0200	0.0720	0.0571	000000	2.0072	3.0072	200000	-0.0431	0.033	-0.0862	\$10.0	0.0072	-0.0200	-0-0863	-0-1073	-0.00ts	-0.0216	0000-0	0.000
0.0047	-0.0186	0.0470	0.0467	-0.0010	-0.0206	0.9072	0.0000	0.0013	-0.0001	-0.0943	0.0133	0.0136	0.0100	-0.0718	-0-1167	-0.030I	-0.0251	0.0018	0.0000
-0.0039	0.0035	0.2111	0.1617	-0-0-27	-0.0047	0.0072	-0-0000	0.0427	0.0740	-0.1949	-0.0285	-0.0025	0.0100	0.0679	0.0395	-0.0715	-0.0499	-0.0807	-0.0000
-6.1464	-3.2600	-5.5420	-10.3547	35.7-	-10.5974	-6.2158	-3.3300	-5.6425	-10.4978	-7.5737	-10.7030	-6,2632	-3.3400	-5.0596	-10.0395	-7.1346	-10.6020	-6.1693	-3.4200
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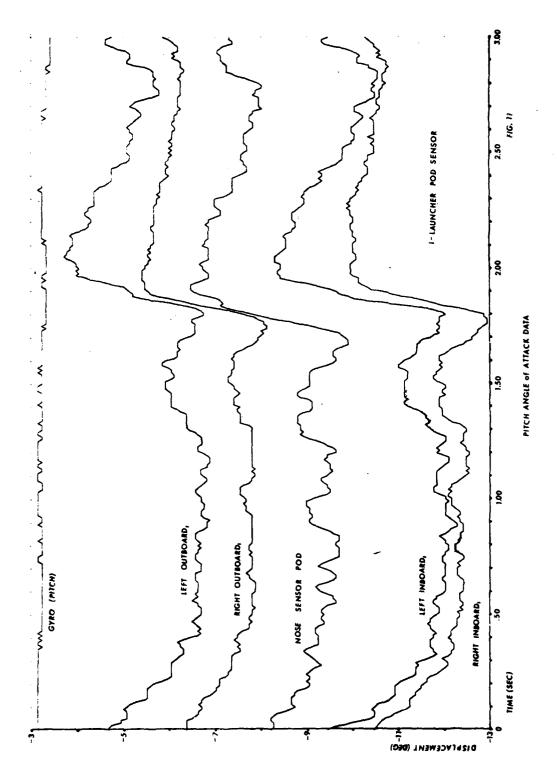
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that there was a pronounced change in amplitude at 1.8 seconds. Since this appears as a ramp signal in the calculation, the Fourier analysis should and did produce a relatively high value for the fundamental and all its harmonics. Due to the number of data points available in one cycle of the signal, calculation of any harmonics above the 4th would be meaningless.

It should also be noted that the gyro pitch (Pitch 6) harmonic coefficient was at or near zero for every calculation. To confirm this result, refer to Figure 11 and observe that there was virtually no variation in this signal.

### 4.1.4 Relative Data Tracking

The developed computer program that was written to perform that analysis on the various sensors also produced a punched card file of the data points under consideration. These cards were run on a digital plotting system for viewing of the data. The results of the gyro pitch and pitch angle of attacks are shown in Figure 11.

The plots show exactly what was indicated by reviewing the data in paragraphs 4.1.1 through 4.1.3. Examining the plots, it can be seen that the aircraft was at a very steady pitch down angle which tends to verify a standard deviation of .071. The consistent relative tracking of the sensor dictates the existance of the high correlation coefficient previously calculated. It can be seen that the nose angle of attack sensors led the others by about 0.12 seconds. This was due to the nose sensor being located 13 feet ahead of the launcher sensors. The abrupt change in the airflow at approximately 1.8 seconds would justify the high frequency coefficients calculated during that period.

The yaw gyro and the yaw angle of attack plots are shown in Figures 12 and 13. A review of the plots shows that the analysis presented in Figure 10 is realistic.

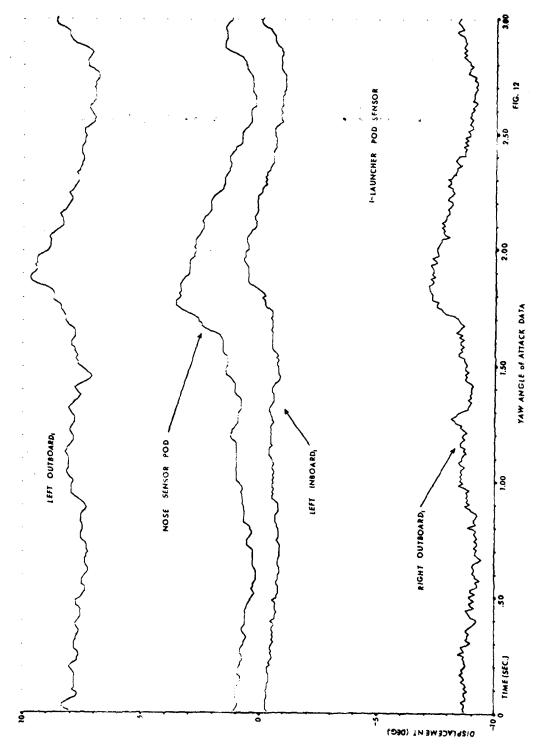
The plots of the Angle of Attack Transmitters were accomplished with corrected data to adjust for the pod offsets as discussed in paragraph 4.1.1.

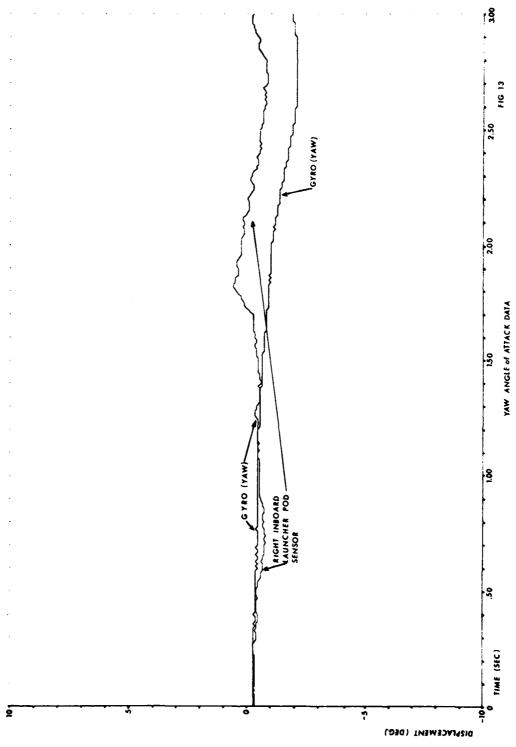
## 4.2 Linear Variable Differential Transformer Analysis

A segment (500 milliseconds) of the raw octal data used in the analysis of the LVDTs is presented on panes 6 through 15. The data, from Run 138, was retrieved on 24 August 1971 on aircraft #67-15691 in a Phase B configuration. The analysis was performed on data accumulated in a three second period immediately following the occurrence of Event Marker #1 (0001 in word D4). The engineering units data listing shows the data frames for the first 0.560 seconds of the three second period (Pg 49-52).

## 4.2.1 Data Statistics

The analysis of the horizontal and vertical LYDT data is shown in Figures 14 and 15 respectively.





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The low mean data values indicate that the sensors were accurately nulled prior to the test flight and remained nulled throughout the sampled time.

From the standard deviation it can be determined that 95.5% of the samples for the left/horizontal/forward LVDT are within  $\pm .0638$  inches of the mean. Therefore it can be stated during the sampled period, a straight and level flight, the left forward position of the rocket launcher was moving approximately 0.12 inches in the horizontal plane.

### 4.2.2 Data Correlation

The correlation, as shown in Figure 14, between the horizontal LVDT sensors indicates that the movement in the yaw plane was mainly a rotational motion. The left fore and aft LVDTs have a correlation factor of -.9542 indicating that the front and back of the launchers were moving simultaneously in opposite directions. The motion of the left and right launcher correlates quite well with the forward LVDTs, having a correlation coefficient of +.6354 and the aft LVDTs, having a coefficient of .9165.

The correlation coefficients for the vertical LVDTs are shown in Figure 15. The coefficients between the fore and aft sensors were negative defining a pitching motion as expected. The coefficients were -.3 and -.4 for the right and left sides respectively and the low correlation figure indicates a combination of translation as well as pitch motion in the vertical plane. The launcher is supported at multiple points and therefore the vertical movement is not a simply described motion.

### 4.2.3 Frequency Spectrum Analysis

Calculations of the Fourier coefficients for the LVDTs were performed on the sensor data. The resultant coefficients are tabulated on pages 82 through 85.

The data indicates that there was significant harmonic content in the sampled data. To determine the significance of the harmonics of the 11 Hertz fundamental, the data could be normalized by dividing each of the coefficients by the DC values or the coefficient of the fundamental. For the LVDT #2 (left/vertical/forward), the coefficients for the multiples were large compared to the coefficients of the other data and in relation to its fundamental and DC values. This would indicate several significant harmonics were present in the data.

The coefficients for LVDT #5 (right/horizontal/forward) are approximately 100 times smaller, which can be misleading unless they are compared with the DC and 11 Hz coefficients. The results indicate that the harmonic content was as great as that of LVDT #2.

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•	:		3, 9363	-2, 3145	-7.3436	7.7383	0,0013	2	いらしいっし	0.000
•	13	Ø-	-2.0156	0110	-2.2005	-0-0211	-0.0014	-2.00.0-	-7.0015	-0.0019
٠	٠.	er •	-0.000	9.013€	-2.0357		9.0012	0.9072	2.3044	. 0.005A
۴۰	<u>;</u>	a:	-0.0120	הרניה(	3.3324		-3,000	-0.0159	7.7714	-0.3917
~	13	ď,	-0.0149	0.000	-0.0158		2.00.0	-2.0159	3-3005	0.0008
4	c :	æ (	-7.0131	10°0	-0.0947	40.0	-0.0037	0.0256	0.0048	-0.0023
•	13	O' (	-0.0337	-0.0126	2.2267		-7.9303	9:00 D	-0.0065	-0-3942
٠.	6.	e !	-0.0373	7.0043	-0-0045		1000-0-	0.0395	-7.7357	0.0027
(	ř (	2 !	0.0360	9610-0-	1010°b-		-7.0014	66.0	0266	0.0038
~ 4	2			0.0203	82CC-0		0.000	10.0	2100.0-	-0.0004
•		: :		7100-0-	0.30		2000	0.00.0	0.00	670000
•			9710-0-	2000	0.00		6160	4 10 C	7.00	A 200 C
4 •	. •	, [	-0-0131	- A- M264	0.00		5000		- B. M. T.	0.00.0
· «		, (	1150-0-	-0.123			2	1990	100.0	
₹	6		-0.0370	0.00.0	-0-066		0.00	4900-0	00.00-0-	0.0047
•	6.	36	0.0351	-3.3250	2.0114		-0.0003	0.0334	1600-0-	0.0064
L.	23	36	-0.0154	9-0264	-0.000		2.0017	-0.0407	5.3001	-0.0021
4	6.	92	4006-0-	-0.0312	-0.0049		-0.0006	9-0069	5.0013	-9.0004
• 1		9	9110-0-	3.3964	-0.3306		-0.0002	-0.0121	0.0040	2000-0
~	58	2	-0-0158	0.00	0.010		0.0017	-0.0170	-9.0051	0.0079
•	<b>S</b>	2	B 0	-0.02	9000		0.0032	0.0163	0-0032	-0-0055
•	2	<b>9</b> . 7	7260-0-	-0-9113	1000		0.0010	-0.000	B106-0-	-0-0035
٠.	67	D 4	3000 C		00000		1000-0		70.00	
. 10	, F	5	-7.0150	0,7452		-0.0034	200.0	-0.0373	0.000	<b>1000</b>
1 6	4	. 4	-0.0016	-0.4033	-0.0042	-0-0048	-0.00	0.00	-0.0076	- 7.0310
-	37	<b>W</b> .	-2.0123	0.0000	-0.702	0.0007	0000	-0.2126	0.0031	-0.0019
~	LÉ	₩.	-0.0151	₹600.0	-0.0124	-0.00%	-0.0031	-0.0137	-0.0087	9-1065
*	33	<b>*</b>	-0.0118	-0.0319	9.0019	-0-00Je	9.0063	0.9093	-0-9014	-0.000
•	37	<b>\$</b>	-0.0319	-0.MIA	0.4079	0.0059	0.0002	-0.0020	0.3034	-0.0010
	11		-0.0367	0.0032	3.0000	-2.0037	0.0003	2.005	20.00	7.0017
(	\$:	r in	0.0366	-0-0354	-3.0964	-0.0026	0.0017	0.0	-9.09.00	0.0048
* N	;	<b>!</b> :	-7.0156	1660-0	7066-6-	820G-G	*DGO *O-	-0.0283	6100	2666-0-
, •	÷ -	<b>.</b>	6600.0-	-0.003	0.0030	-2.0013	-0.0050	20.0	£260°0-	-0.0059
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•	4	ď	0.010	-3.0102	0.0078	7.0073	0.00	1900	146	0.00
•	4	*	-0.0380	0.0016	0.0075	-0-0047	4600-0-	0.00	-0.0054	-0.034
` <b>p</b> -	. 5	*	0.0344	-9.9385	-0.0022	1600	-0.0013	0.0157	-0-9114	-0.000
	£.	6.9	-7.01%	9-0432	2,0011	-2.00%	1000-0-	-0-01 79	-9-0022	-0-0017
80	53	63	-0.0014	-0.0053	-0.0034	-0.0002	0.0003	0.0362	4500-6-	-0.0046
^	*	63	-0.0124	0.0110	-7.9030	9100°C	0.0010	-0-0115	0.0	0.0002
,	53	63	-0-0189	0.0110	-0.0027	-0.0128	-0.0038	- 0. C	4.0	-0.60
•	\$6	<b>6</b>	-0.0122	-0.03%	1900-0	-6.0321	0.00	-0-0034	-2.0026	-0.0310
ا ڪر	£ ;	3	-0.0910	-7.0061	0.60%		-0.0007	-0.0065	0.000	0.0067
7	£ 4	₽,	-0.030+	0.0002	0.000	*000°0-	-6.98%	0.0000	-9.0054	-100°G-

0.0001	0000	2.000	7,000	2.0319	-7,7215	-0.00.E	60003	1000	2,0014	1.0021	0.0030	-0.0012	-1,3025	2.000	-9.0026	-0.0006	2000-0	- 3-9917	0100.0	-0.0037	3.9904	-0.0016	0.000	2000-0-	0000	0.00	-9.0001	0.0007	-0.0002	-0.0001	41CO - C-	-0-0034	0.0021	0.0016	900	0.00	-0.0000	-0.0009	-7.0314	2000	-0.000-	2.0024	0.7014	-0.0704	00000	100.00	0.00	-0.000	0.0011	0.0000	0000	- 0.000
-0.0010	-0.00e	7,7312	2.250+	-1.000-	7,1975	-3-1054	7,0054	3505	7, 7912	-7.1340	2,000	9.3975	-2.3033	-0.03	7.1004	-0.000	7.033	- 100.00	0.7029	-0-0040	-0-0005	2.0012	4.0064	0.9015	00000	1000	2.3319	-2.3013	9. 9304	9-2056	10.00	-7.302E	-0-0073	2.0027	2100.0-	0.0056	-0.3006	-0-004	-0.9921		7.7048	P.0917	3.2035	-0.9013	0-000		0.000	0.003	-0-0013	0.000	-0.0023	5 6 0 0 ° 1.
-0.0095	0.00.0	0.000	-0.2174	-0.001	30.30	-0.000	10.00	-0-00-0-	2000.0	-2.0134	-0.0030	0.0072	0000	-0.006	2.004.4	20000	-0.036	0000	0.0093	0.0083	-0.002m	-3-0003	-0.0055	2600-0-	770000	# 100 C	0.0054	-0.0001	0.0012	-0-0013	-0-00-6	0.000	0.0033	0.0103		0.0007	-0.002	0.0117	-0.0004	100.0	0.0047	0.000a	-0.0001	-0.001	6200-0	100.00	0.000	0.0114	-0.0001	0.0041	-0.0034	00200
0.0066	0.0075	-0-10a2	-7.4705	-0.0043	40°C-	3,7243	7,075	0.0063	-7.2244	-7.7944	-3.0117	-0.0101	0.9924	-0.0067	0.0034	200	-0.0065	-0.0167	-0.0102	0.0033	-0.0123	0.0134	0-0027	2000-0-	2000	1000-0-	0.3924	-0.0219	0.0227	0.0034	0-0039	-0.0244	-0.0103	0.0024	1520-0-	-0.0002	9.0035	0-0069	-0.0336	2010-0	-0.0346	2010-0	-0-0051	0.0110		-0.091	00.0	-0.0386	0.0473	-0-0056	0-0111	70 00 00
0.000	-100-0-	1.00%	5,00,0	700000	71.00 L	-7-7732	במניני בר-	-0.933	-0.0032	-7.0929	-7-3371	0.000	10.00%	-7- 7001	-0.0001	01000	35.5	-0.0033	-0.0006	0.0027	9100-	0.0012	5200-0	7100-6-	4000	-0-00-1	0.0041	2.0004	0.0041	9000	7.0016	1400-0	-0.0010	0.0036	100.0	0.00	9.0012	-0.0005	0.000 c	3000-C	0.0001	J. 0030	0.000	7.00.0	2000	6000	-0.00	-0.0000	-0.0014	-0.0005	90000	41614
-7.0021	7-0007	2,2917	7FC0.1-	2.0012	2.111	-0.0.6-	24.C.C.	7.976	-7.1172	-0.030	<b>~0°003</b> 0	-7-774:	3.5021	AC0004	F100-0	2000	-0.000-	3.0011	-0.0047	0.0019	2.0007	-0-0012	0.0054	100.0	1000	CE 10.0-	3.0354	7.9061	0.0018	0.00	20010	0.000	-3.9942	0.0022	200	-0.000	-0.9034	2.0051	-7.00	2,000	0.0043	0.0039	1.00.0-	90000	666	2000	0.3011	0.0024	-0.0010	-0.0053	-0-0002	3.5
5.0013	13.93	-3.33	7.00	-1.0323	2,2313	7,0107	0.0010	0.0002	-1.79.2	3,013*	1.0973	0.0013	0.000	3.3356	-1.0924	6100.0	7,009A	-0.3042	-0-0020	0.0091	0.0193	7.0024	1600-0	42 DE -0-	45.00	-0.0050	3,3049	9.3057	-0.0013		9.0154	-3.3325	-0.0197	0.0026	60000	0.0360	0.0905	0.0143	0.3025	500	0.0954	0.271	2.0047	7.0047	0.00	2000-	-0.0063	92000	0.000	0.0025	1000	• • •
-0-1393	-0.797	7,3164	1.9127	-9.3760	-0.3056	-3.033	7,1516	-0.3960	2,3139	5-316-0	-7.3234	-0.0041	-0.0004	-0.0412	0.0633	0.010.0	0.0149	-0.0212	-0.0022	-9.9051	-7.0444	0.0494	-2.0105		-0-0244	-0.0036	-7.7950	1660-0-	0.0498	9210-0-	0.014	-0.0240	3.9733	-0.0046	4760-0-	-0.0106	0.01 %	0.0128	RF 10.0-	-0.0010	-0.0275	0.0354	-0.0128	9-0132	0020-0	2010-0	-0.0050	-9.0249	0.0307	-0-0064	0.0135	1910-0
0.0354	-7, 70; 4	-2, 7124	-3.0157	-9.01.6-	-0.3317	-2.0293		-2.2014	-3.0121	-0.0164	-7.3133	-0-630	-2.0348	0.0346	6410*6-	0100	-3.0161	-0.0134	-3.0300	-0-0386	0.0350	-0.0169	-0.0004	20.00	10.0109	-0-0314	-0-0354	0.0349	-0.0154	-0-000 -0-000	-0.0157	-2.0134	-0.040e	-0.0374	7666.C	-0.0005	-0.0136	20.0	-2.0139	0560-0-	0.0350	-0-01 és	-2.0012	-7.0129	44.6		-0.048B	0.0337	-0.0150	-0.0010	20.0	D 15-5-
2;	2	, <b>t</b> ,	<b>F</b>	ţ	ţ	}";	, ,	: 6		ā'	n.	<b>a</b> 1	<del>,</del>	r (	<b>5</b>	F 6	) F	6	00	Ş	8	8. (	<b>3</b> i	, ş	8	ę	00	#:O:	100	8		80.	129	÷01	121	117	111	117	117	111	124	126	126	126	57.	126	125	135	135	<u>\$</u>	, , , , , , , , , , , , , , , , , , ,	261
33	4	*	*	7	74	7		73	F	4	Ė	ŗ	<b>!</b>	26	N E	is e	. 6	9.	ç	92	6	6	5 7	7 8	7 6		, <u>1</u>	100	100	2	200	001	6	100	601	8	103	109	<u> </u>	100	119		114		0 6			127	121	127	127	171
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### 4.2.4 Relative Data Tracking

Profiles of the vertical and horizontal LVDTs are shown in the data plots, Figures 16 through 23. The 11 Hz fundamental frequency is apparent in all figures.

Examining Figures 13 and 20, it is apparent that the harmonic content was considerable for the LVDTs as was discussed in paragraph 4.2.3.

The degree of movement of the launchers can be determined by calculating the magnitude of the peak values from the plots.

The curve connecting the positive peaks of the LVDT (LVA) data plotted in Figure 21 and the negative peaks of the LVDT (LVF) data plotted in Figure 20 were parallel consistantly over the interval of time shown. This parallel envelope movement indicates that translational motion of the launcher occurred during the normal flight. The plot indicates that the launcher translated approximately .014" (See Figure 24).

The peaks described within the envelope indicate that the front of the launcher peaked in one direction, while the rear of the launcher peaked in the opposite direction. This indicates a significant amount of rotational motion. From the curves it was determined that the launcher oscillated within approximately a l mil excursion. The combination of the translational and rotational motion caused a complex launcher motion that would result in low correlation coefficient for the LVDTs.

The rotational velocity of the launcher pod can be calculated from the slope of the LVDT curve. The calculation for the left launcher indicates the launcher rotates at a rate of approximately 100 mils/second.

# 4.3 Accelerometer Analysis

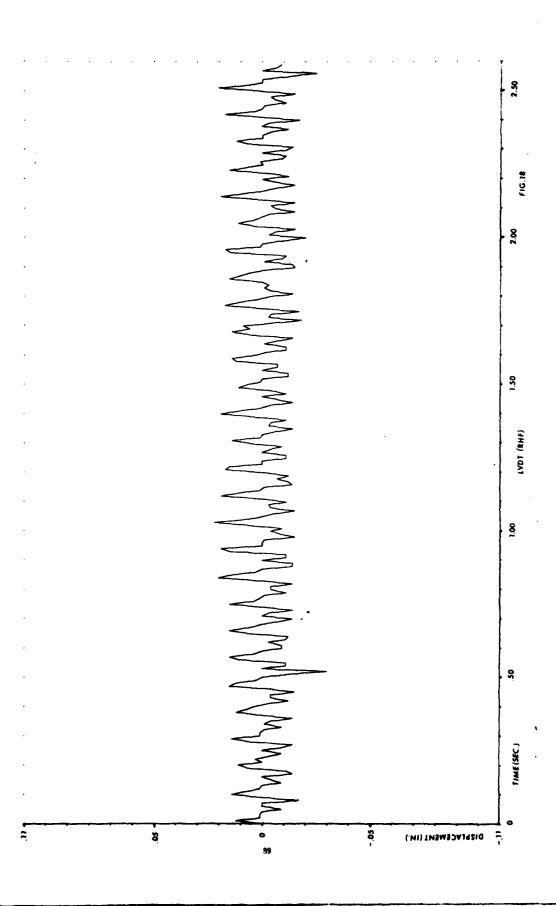
The data used for the analysis of the accelerometers is shown in the data frame of the engineering units printout, pages 49 through 55. The flight data was described in paragraph 4.2. The accelerometers are sampled 10 times per frame/1000 times per second and the analysis was performed on the first 260 data points. This data was retrieved in 0.260 seconds, all of which is presented in the first 26 data frames of engineering units printout.

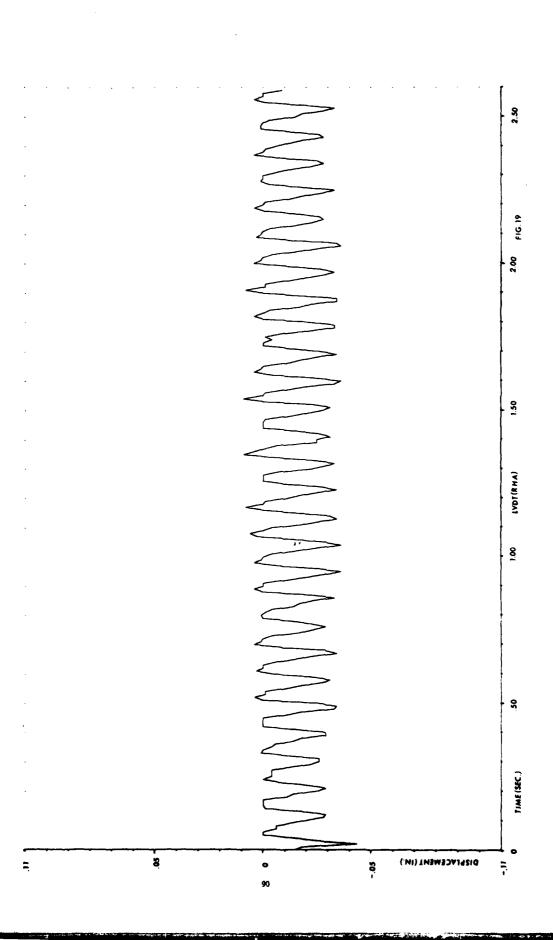
### 4.3.1 Data Statistics

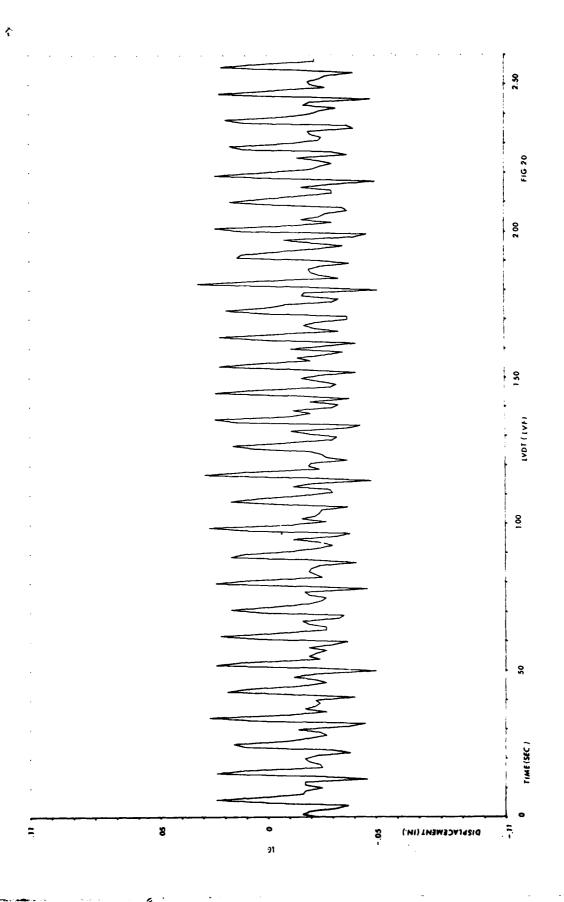
The accelerometer data analysis is presented in Figure 25.

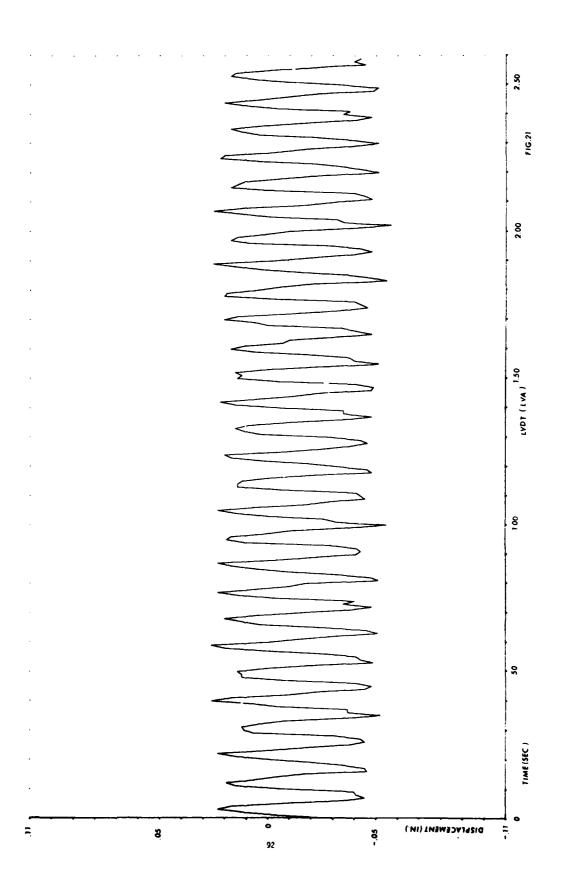
It can be seen from the data that the mean values for the lateral and fore/aft acceleromaters were -0.2336 and +2.9330 ft/sec² respectively, indicating a lack: of predominant acceleration in the left, right, fore or aft direction. This was consistent with the known straight and level flight profile. The high RMS and standard deviation indicates that the

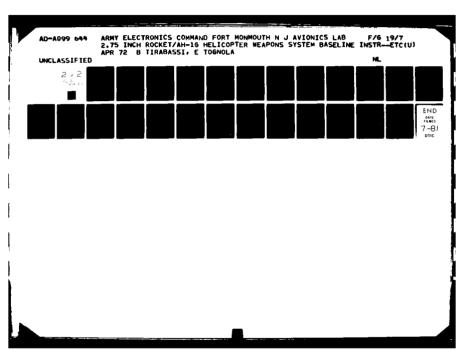
2.50 FIG. 16 2.00 1.50 LVDT (LHF) 8 DISPLACEMENT (IN.)

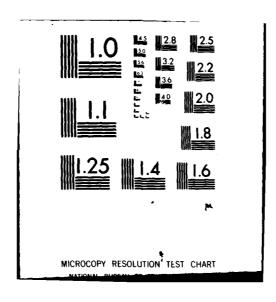


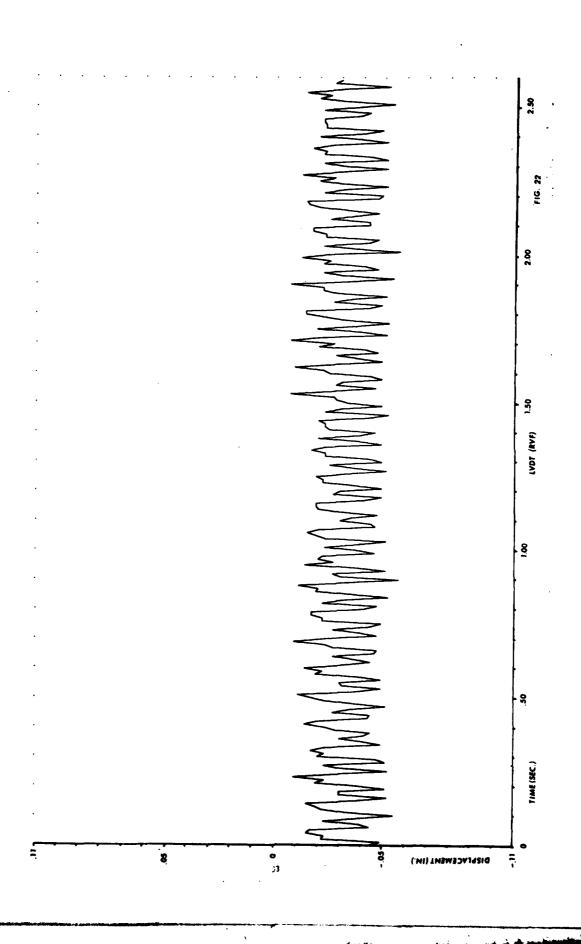


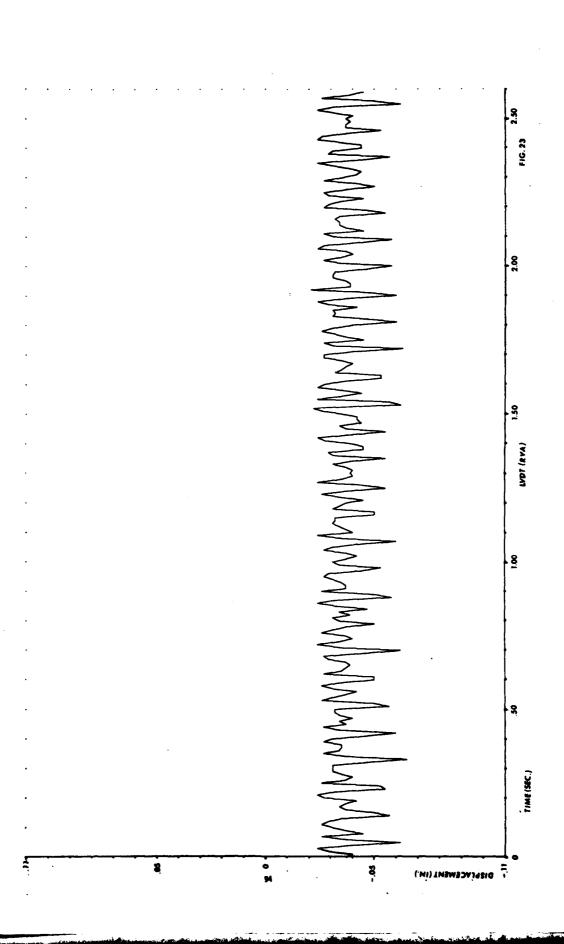


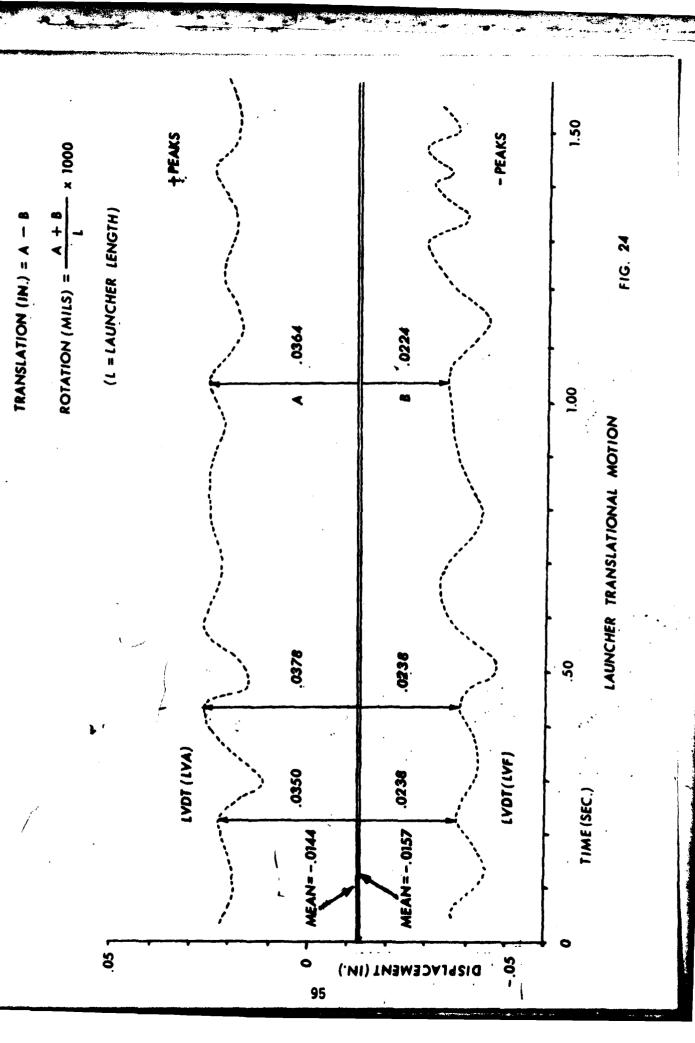












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aircraft was experiencing considerable acceleration in all directions (about 1/3g) but was cyclic as shown by the True mean value.

The RMS value for the vertical accelerometer (ACCUD) was 32.4141 ft/sec², consistant with the normal gravity vector.

## 4.3.2 Frequency Spectrum Analysis

The Fourier coefficients for the accelerometer data are shown on pages 98 through 103.

It can be seen that the harmonic content of the data is significant up to approximately 55-Hz.

# 4.3.3 Relative Data Tracking

The relative data tracking of the accelerometer data is shown in Figures 26, 27, and 28. The accelerometer data was sampled on a DAU high rate channel (1000 samples/second) and therefore many more points per cycle were available for analysis. Only the first 260 data points (0.26 seconds) were plotted.

It can be seen from the plots that the acceleration was cyclic and did vary over a considerable range.

## 4.4 Trigger and IR Detector Analysis

The data for the analysis of the trigger and IR detector analyses is presented on pages 107 thru 116. The data was retrieved during the Phase B flight on 24 August 1971, previously described in paragraph 4.2.

The trigger pulse was indicated on channels Al and A5 by a pulse of approximately 1.5 volts with a duration of approximately 1.5 ms. The rear IR detector produced a -1.5 volt pulse when the IR in the plume of the rocket was detected. The forward IRs produced a -0.5 volt pulse when the IR was sensed.

To determine the delay characteristics of the rocket system and the average velocity of the launched rocket, the Al and A5 channels were monitored for the pulse and the times of occurrence noted. The Al channel monitored the left detectors and the A5 channel monitored the right side detectors.

## 4.4.1 System Delay Characteristics

The octal reading for channels Al and A5 of 4036 and 4011 respectively represent the ambient analog noise level on the channels. The channels were monitored for the trigger pulse represented by a significantly larger voltage level.

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0.0347	-3.9431	TAL, STA	3.9563 -0.4478	0.0742 -0.1451	-0.0368	-0.0216	VTAL, STA	-0.7136 -0.3023	-0.1781	-0.0499	-0.0499	VTAL, STA	
0.3263 -0.3287	-3,3753		2,7409	0.3984	-6.9626 -6.0981	-0.0567		0.4199	-0,3259	-0.1194	-0,0753		
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-3-2536	-0.2200	-0.2164	-0.2919	-0.3247	-0.1252	-0.3115	-0.1862 -0.2970	-0.2970 -0.2125	-0.2310	-0.2360 -0.0731	-0.3276 -0.1053	
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5.0	-0.5672	2.5869	-7.4150	-4,2277 -9,0953	-0.09!!	-0-1163 0-4889	2,1227	-0.1359	0,3041	0.1910	0.7089	
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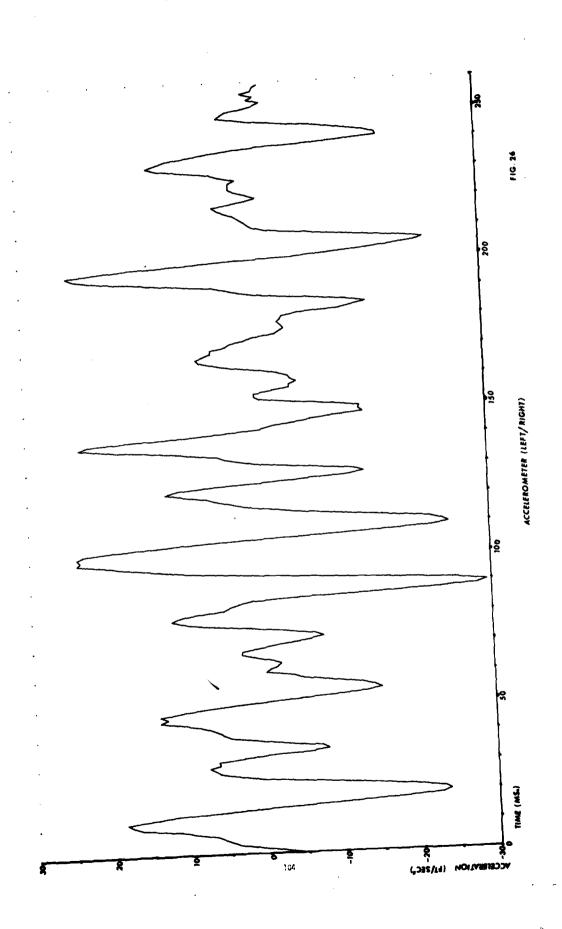
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0.0289	0.0135	0.0290	-0.0240	0.0374	-0.0437	-0.0645 0.0010	-0.1763	-0-176g 0-0423	-0.0408	-0.0786 7.0462	0.0269
-0-1143	-0.0135 -0.0041	-0.0209	0.0123	-0.0233 -0.1409	0.1322	-0.0721	-0.0332	0.0066	-0.0946		
URIER C	FOURTER COEFFICIENTS 494 FOURTER COS AND SIN COEF	EMFS KOR ACCLE, 11 HZ SIR COEFFICIENTS	CLR, 11 H IENTS		NTAL. STA	FIPODAMENTAL. STARTING WITH	H WUMBER	365		;	
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1.1302	0.0240	0.2551	0.3410 -0.5135	-0-1776	0.0048 -9.0241	-0.2409	9.1546	0.0365	0.1549	0.1596	-0.1301
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0.0733	- 3.0658	-0.2369	-0.2544	-0.0375	-0.1346	5190-0-	-0-1522 -0-0-66	0.1205	0.0211		

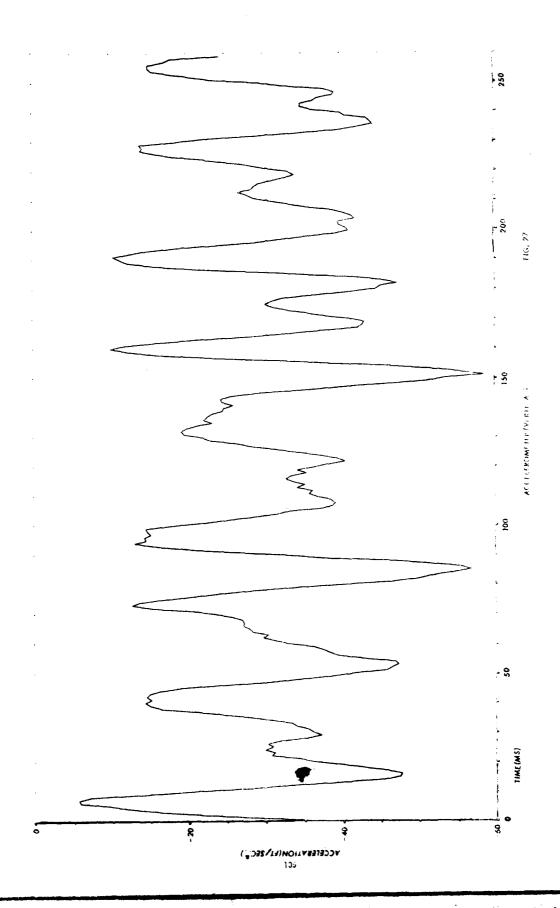
-6.2657 2.541 -4.4056 -2.3717 6.4492 0.1945 -2.1044 0.4491 0.4466 -0.6146 -0.5352

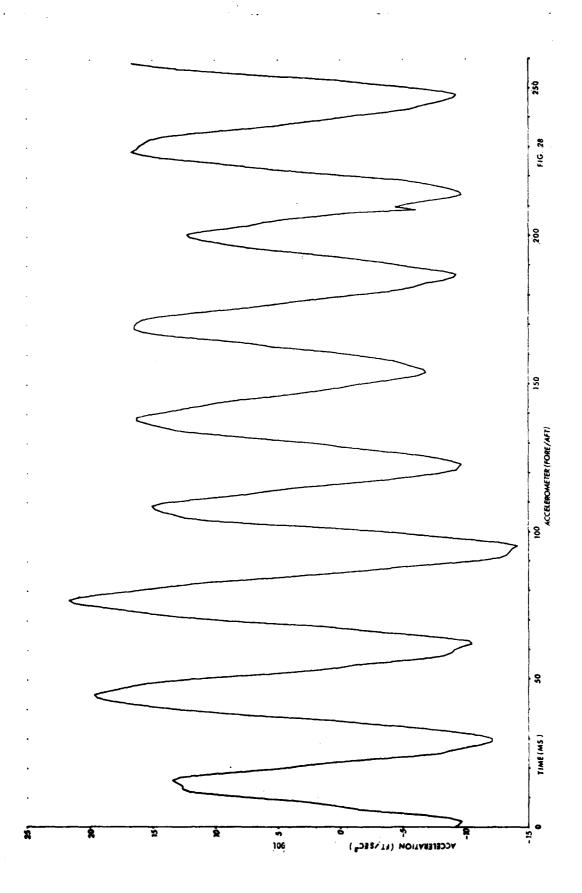
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and and	CONTINUE CULT THE SAN AND SAN A	My Six Coefficients	TENTS	DECASS 24	NTAL . ST.	RINGBARRATEL STABTICS ELTS AGENTE	asumin H	-		·	
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0.747: -7.1074	-0.224	-3-1-6- -3-13-6-	-0-3*45 -0-1425	-0.1447	-0.2644	-0°1674	-9.1574 -0.0265	+0.2745 0.0454	-2.1278	-0.0647	-7.1449
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102	0.9050	4.8108	-3.9784	5.5866 4.6775	-0.4069	7,1859	3.5005	0.1045	-9-295-	0.3267	-6.2724
9.0504 0.837	3.1347	3.1281	-0.0656 0.5035	0.1015	0.0990	7.2321	9.2405	0.1001	0.1637	0.34.0	0.1150
0.1360	7.2095 0.1706	0.2051	0,0263	0.2194	0.1285	0.0642 0.1344	9-1115	0.2122 -0.3066	94££.00 910£.00	0.4003	-0.0246 -0.0796
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FOURTER COEFF	DEFETCTEN	IFIENTS FOR ACCUD. 11 MP NO STW COEFFICIENTS	100. 11 H	7 FINDAME!	WTAL, CTAG	elingamental, staqtim6 bitH .njmqfe	astorii.	1.83			
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-0.0451	96139	-0.2366	-0.1807 0.0537	-0.0169	0.0527	0.2208 -0.0270	3.0440 9.1449	-0-1751	-0-7349	-0.1627	0.0885

7 0.1227 -0.0132 - 1 H7	-0.1103 -3.0538 -5.0423 -3.3524 -0.0248 0.3883 0.3107 -3.3257 FUNDAMENTAL, STRATING ATTH MIMBER	-0.0423	-3-7524				
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The trigger was detected in the data frame, time 11.6310, on channel Al.

In the data frame time, 11.9010 the IR detector sensed the rocket plume indicating that a rocket had cleared the right launcher. In the following frame, it is indicated that a rocket had cleared the left launcher.

To determine the rocket egress delay characteristic the time difference between the trigger and the first IR pulse was obtained

DELAY (right side) = 11.907 seconds - 11.631 seconds

≈ .276 seconds

DELAY (left side) = 11.916 seconds - 11.631 seconds

≥ .285 seconds

This delay time was found to be typical of most firing runs.

## 4.4.2 Rocket Velocity Determination

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The forward IR was located 60±1 inches forward of the rear detector. Therefore the average velocity can be obtained by determining the time taken to traverse the distance.

The occurrence of the 2nd IR pulse was indicated in data frame time 11.951.

The average velocity of the rocket fired from the left launcher is determined below.

The average velocity of the rocket fired from the right launcher is determined below.

VELOCITY = 
$$\frac{5 \text{ ft}}{11.954 - 11.907}$$
  
=  $\frac{5}{.047}$  = 107 ft/sec

These values were found to be typical of most firing runs.

